



**EVERGREEN DESIGN COMPANY**

**Structural Calculations  
for the  
Ravensdale Residence**

Location: 310<sup>th</sup> Avenue SE, Ravensdale, WA 98051

Prepared for: Lane Williams Architects

Prepared by: Lori D. Brown, P.E., S.E.  
Structural Engineer

Date: October 21, 2019



**Project:** Ravensdale residence

**Design Criteria:** 2015 International Building Code  
Assumed allowable soil pressure 2000 psf

**Live Loads:** Roof 38 psf (Snow load, drift to 60 psf)  
Floor 40 psf

**Dead Loads:**

Roof:	Roofing	3.0	
	5/8" plywood sheathing	1.8	
	Prefab trusses @ 24" oc	3.0	
	Mech/Elect/Misc	0.5	
	5/8" gypboard	2.8	
		<hr/> 11.1 psf	Use 15 psf
First Floor:	Finish flooring	4.0	
	3/4" plywood sheathing (or 1-1/8")	3.3	
	11.875" TJI 360 @ 16"oc	2.3	
	Mech/Elect/Misc	0.5	
		<hr/> 10.1 psf	Use 12 psf
Interior walls:	2x4 studs @ 16"oc	1.0	
	5/8" gypboard ea side	5.6	
	15/32" Plywood	1.5	
		<hr/> 8.1 psf	Use 10 psf
Exterior walls:	2x6 studs @ 16"oc	1.6	
	5/8" gypboard	2.8	
	15/32" plywood	1.5	
	Exterior siding	3.0	
		<hr/> 8.9 psf	Use 10 psf

**EVERGREEN DESIGN COMPANY, PLLC**1044 Wyndham Way  
Camano Island, WA 98282JOB RAVENSDALE

SHEET NO. \_\_\_\_\_ OF \_\_\_\_\_

CALCULATED BY UB DATE \_\_\_\_\_

CHECKED BY \_\_\_\_\_ DATE \_\_\_\_\_

SCALE \_\_\_\_\_

SNOW LOAD

Elevation 825'

Isoline 0.054

$$p_g = 0.054 \times 825' = 45 \text{ psf ground snow}$$

$$C_t = 1.0$$

$$C_e = 1.2 \text{ (Exp. B sheltered)}$$

$$I_s = 1.0$$

$$p_f = (0.7)(1.2)(1.0)(1.0)(45) = 38 \text{ psf flat roof snow}$$

Drifted snow at parapet (3')

78' width Fig. 7-9 ASCE 7-10

32' width Fig. 7-9 ASCE 7-10

(see following page)

60 psf max drift

8.75' drift width

**ASCE 7-10 Snow Loads**

File = C:\LORICA-1\Enercalc\Ravensdale.ec6

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Description: Ravensdale

**Flat Roof Snow Loads**

Description:		per ASCE 7-10, Chapter 7	
Ground Snow Load, per Fig 7-1	45.00 psf	Roof Slope, Sec 7.3.4	0.00
Terrain Category	B (see ASCE 7-10 Section 26.7)	Roof Configuration	Monoslope
Exposure of Roof	Sheltered		
Ce : Exposure Factor, Table 7-2	1.20		
Ct : Thermal Factor	1.0 : All not otherwise defined	pm, Minimum required	20.00 psf
Risk Category, per Table 1.5-1	II	pf, Calculated Snow Load per Equation 7-1	37.80 psf
Importance Factor, Is, Table 1.5-2	1.00	pf, Design Snow Load Max(pm min, pf calc)	37.80 psf

**Snow Drifts on Roof Projections**

Description: Longitudinal		per ASCE 7-10, Chapt	
Balanced Snow Load	38.00 psf	hd : windward	2.63 ft
Ground Snow Load	45.00 psf	hd : Design	1.09 ft
lu-upwind	78.00 ft	pd : Max Drift Only	21.55 psf
Height of Projection	3.00 ft	pd + Balanced	59.55 psf
Snow Density	19.85 pcf	W : Drift Width	8.69 ft
hb : Balanced	1.91 ft		
hc : Ht. of Projection - hb	1.09 ft		
hc / hb	0.57		
Description: Transverse		per ASCE 7-10, Chapt	
Balanced Snow Load	38.00 psf	hd : windward	1.66 ft
Ground Snow Load	45.00 psf	hd : Design	1.09 ft
lu-upwind	32.00 ft	pd : Max Drift Only	21.55 psf
Height of Projection	3.00 ft	pd + Balanced	59.55 psf
Snow Density	19.85 pcf	W : Drift Width	8.69 ft
hb : Balanced	1.91 ft		
hc : Ht. of Projection - hb	1.09 ft		
hc / hb	0.57		

# Design Maps Summary Report

## User-Specified Input

**Report Title** Ravensdale

Mon October 8, 2018 18:27:32 UTC

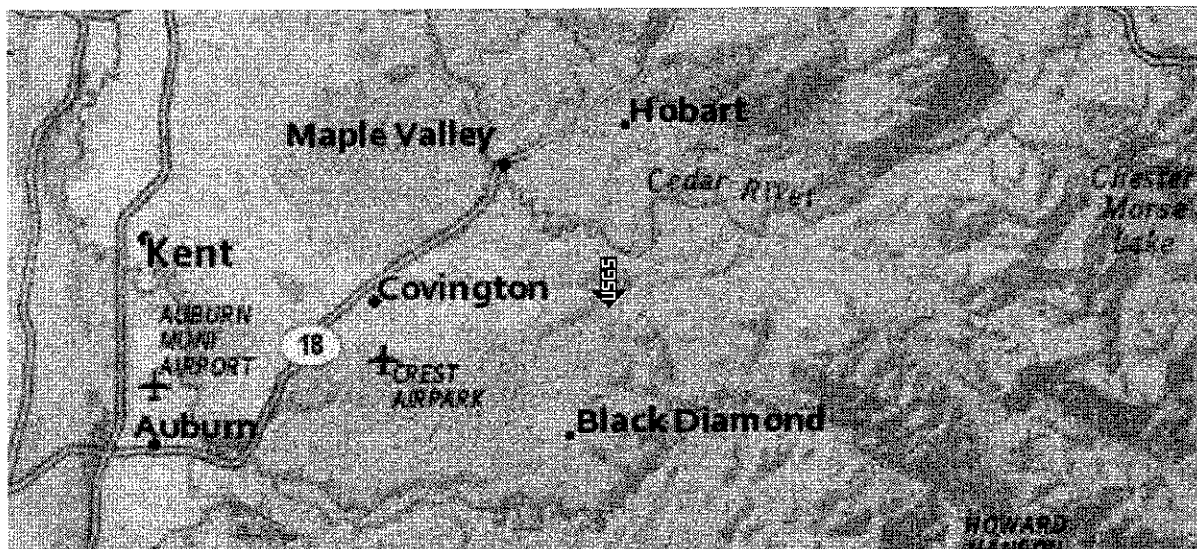
**Building Code Reference Document** ASCE 7-10 Standard

(which utilizes USGS hazard data available in 2008)

**Site Coordinates** 47.3642°N, 121.9831°W

**Site Soil Classification** Site Class D – “Stiff Soil”

**Risk Category** I/II/III



## USGS-Provided Output

$S_s = 1.193 \text{ g}$

$S_{MS} = 1.220 \text{ g}$

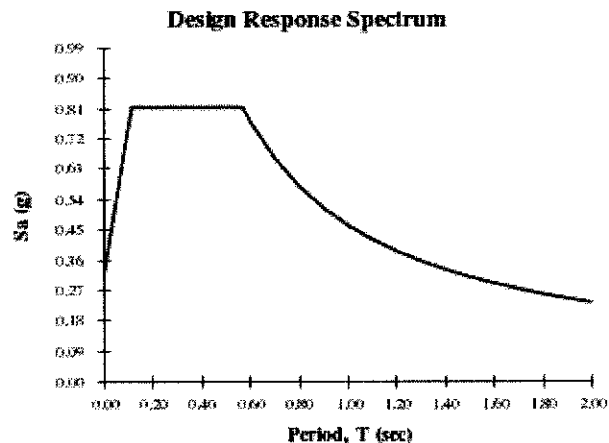
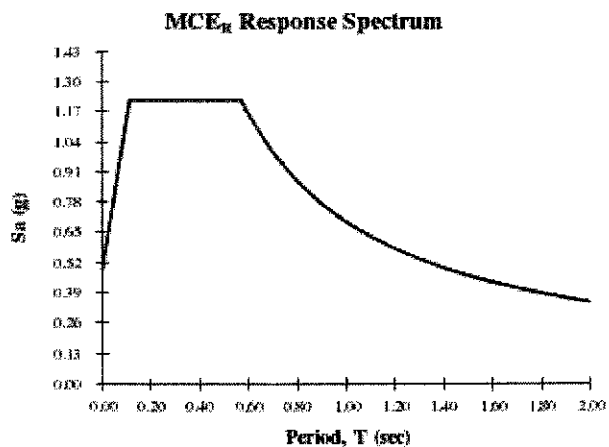
$S_{DS} = 0.814 \text{ g}$

$S_1 = 0.448 \text{ g}$

$S_{M1} = 0.695 \text{ g}$

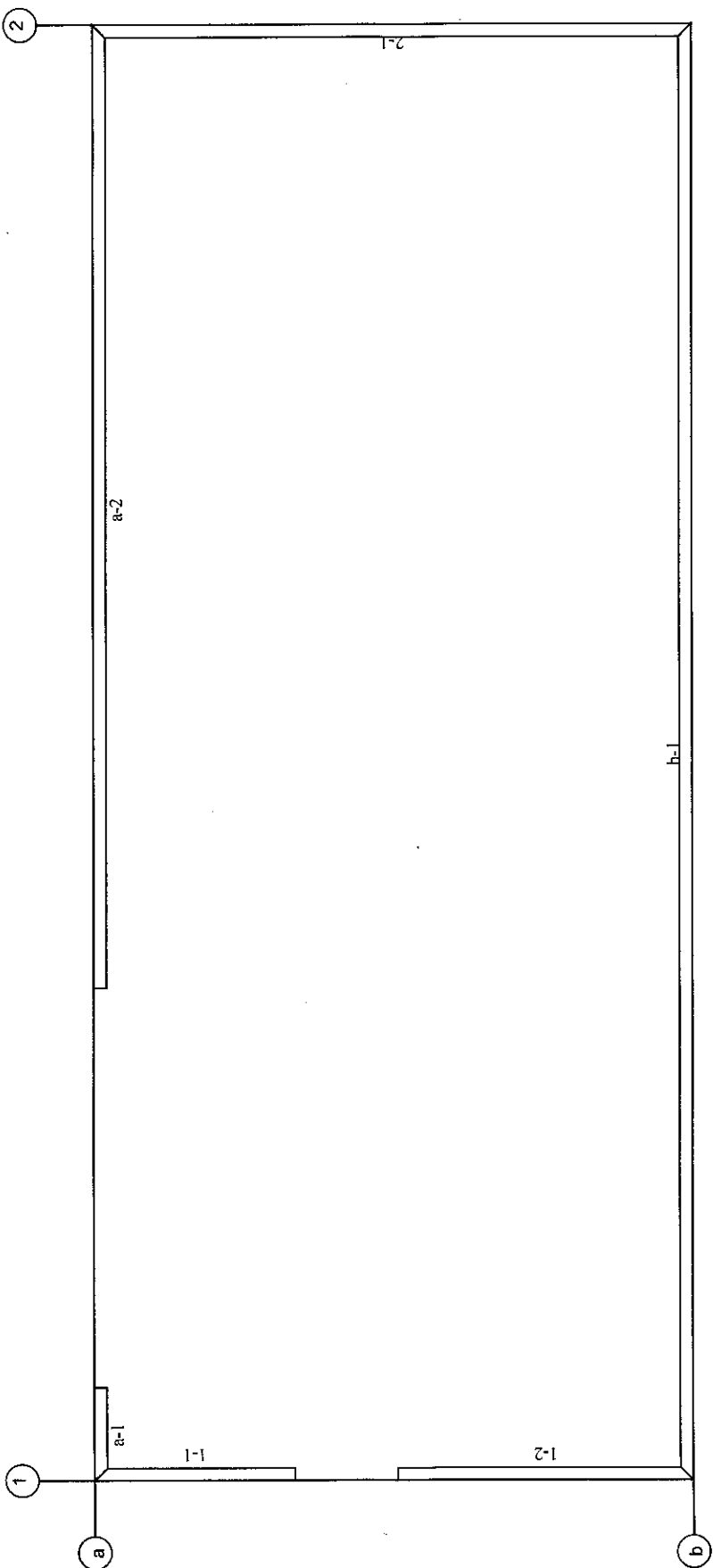
$S_{D1} = 0.463 \text{ g}$

For information on how the  $S_s$  and  $S_1$  values above have been calculated from probabilistic (risk-targeted) and deterministic ground motions in the direction of maximum horizontal response, please return to the application and select the “2009 NEHRP” building code reference document.

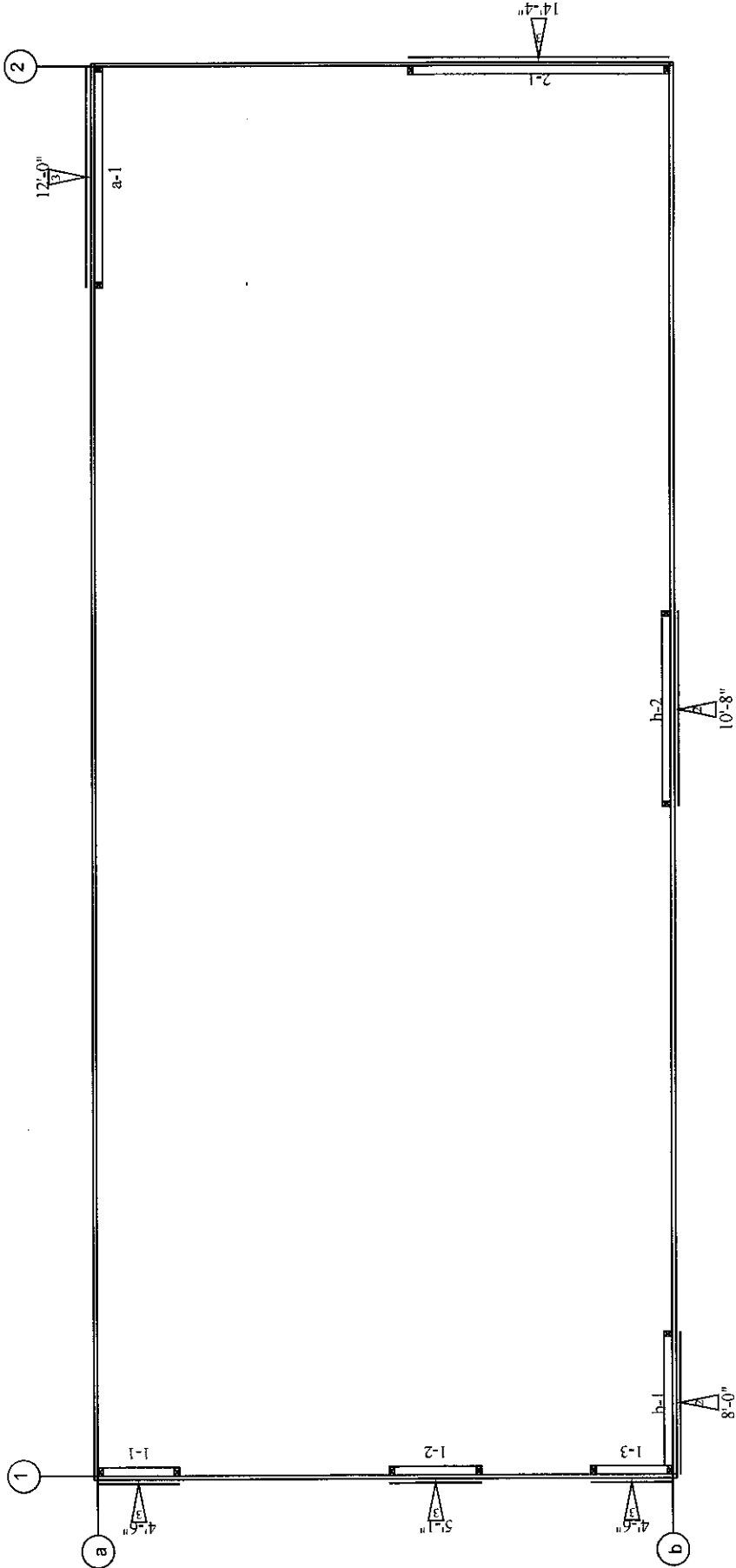


For  $PGA_M$ ,  $T_L$ ,  $C_{RS}$ , and  $C_{R1}$  values, please [view the detailed report](#).

SHEAR WALL LAYOUT OF (1ST)



SHEAR WALL LAYOUT OF (2ND)



Evergreen Design Company		DESIGNED _____	JOB NO. _____
PROJECT	Ravensdale	CHECKED _____	SHT _____ OF _____
SUBJECT	_____	DATE _____	

### Building Information

No. of stories 2

Building height for lateral calculations (ft) 21.77

Building weight (lbs) 121159

Redundancy Factor:

N-S: 1.3

E-W: 1.3

### Floor Information

Floor\_ID 1st

Floor net area (sf) 2382

Floor opening area (sf) 114

Average height (ft) 9.00

#### Diaphragms

Floor diaphragms for 1st									
Diaphragm name	Area (sf)	Effective seismic weight (psf)						Type	Remarks
		DL	Walls	Snow	Storage	Partitions	Total		
D1	2382	12.00	10.00	0.00	0.00	0.00	22.00	Floor	

Floor\_ID 2nd

Floor net area (sf) 2491

Floor opening area (sf) 0

Average height (ft) 9.00

#### Diaphragms

Floor diaphragms for 2nd									
Diaphragm name	Area (sf)	Effective seismic weight (psf)						Type	Remarks
		DL	Walls	Snow	Storage	Partitions	Total		
D1	2491	15.00	5.00	7.60	0.00	0.00	27.60	Roof	Ignore opening in weight calculations



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<b>SUBJECT</b>	_____	<b>DATE</b> _____		

### Seismic Loads

Design code 2015 10  
~~2009~~ IBC (ASCE 7-05)  
Lateral force calculation method Equivalent Lateral Force Procedure

### Seismic data:

Building occupancy category	II. Standard	Table 1-1
Importance factor I	1.00	Table 11.5-1
Soil site class	D. Stiff soil profile	Table 20-3-1
Response Spectral Acc. (0.2 sec) ( $S_s$ )	1.20	Fig 22-1 through 22-14
Design Response Spectral Acc. (0.2 sec) ( $S_s$ )	1.20	Fig 22-1 through 22-14
Response Spectral Acc. (1.0 sec) ( $S_1$ )	0.45	Fig 22-1 through 22-14
$T_L$ (sec)	6.00	Fig 22-15 through 22-20
Fa	1.02	Table 11.4-1
Fv	1.55	Table 11.4-2
Max. Considered earthquake acc. $S_{MS}$	1.22	(11.4-1)
Max. Considered earthquake acc. $S_{M1}$	0.70	(11.4-2)
Design spectral acc. at short period $S_{DS}$	0.82	(11.4-3)
Design spectral acc. at 1 s period $S_{D1}$	0.46	(11.4-4)
Seismic design category based on short period	D	Table 11.6-1
Seismic design category based on 1 S period	D	Table 11.6-2
Is $S_1 > 0.75$	False	Sec 11.6
Project seismic design category	D	
Seismic force resisting system	13. Light-framed walls sheathed with wood structural panels rated for shear resistance or steel sheets	Table 12.2-1
Response modification coefficient R	6.50	Table 12.2-1
System overstrength coefficient $\Omega_0$	3.00	
Subtract 0.50 of Resistance Factor for flexible diaphragms	True	
Approximate fundamental period parameters	$C_t = 0.02$ $x = 0.75$	Table 12.8-2
Building height (ft)	21.77	
Building period $T = T_a$ (sec)	0.20	(12.8-7)
Regular structure and 5 stories or less?	True	
Maximum $S_{ss} = 1.50$	False	Sec 12.8.1.3
Base Shear Adjustment Factor	1	
Minimum $C_s$	0.01	12.8.5
Seismic response coefficient $C_s$	0.13	(12.8-2)
Adjusted $C_s$	0.13	

**Seismic load:**       $V = C_s W = 0.13 \quad W$

For allowable stress design       $0.7 E = 0.7 * 0.13 = 0.0879 \quad W$

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Total effective weight (lbs) = 121159

Total seismic force (ASD) (lbs) = 10647

#### Vertical seismic load distribution:

$$F_x = C_{vx} V$$

$$C_{vx} = \frac{w_x h_x^k}{\sum_{i=1}^n w_i h_i^k} \quad (12.8-11)$$

$$T = 0.20$$

$$K = 1.00$$

Sec 12.8.3

Floor	Wx (lbs)	hx (ft)	Wx * hx lb.ft	$\frac{Wx * hx}{\sum(W_i * h_i)}$	Fx (lbs)
1st	52396	10.05	526689	0.2603	2771
2nd	68763	21.77	1497031	0.7397	7876

Sum(W)= 121159

Sum(W\*h)= 2023719

#### Diaphragm design force:

$$F_{px} = \frac{\sum_{i=x}^n F_i}{\sum_{i=x}^n w_i} w_{px} \quad 12.10.1$$

Minimum value =  $0.2 S_{SD} W_{px}$

Sec 12.10.1

Needn't to exceed =  $0.4 S_{SD} W_{px}$

#### Diaphragm seismic forces:

Floor	Sum(Fi) (lbs)	Sum(Wi) (lbs)	Wpx (lbs)	$\frac{\text{Sum(Fi)}}{\text{Sum(Wi)}} W_{px}$	Min. Value	Max. Value	Fpx (lbs)
1st	10647	121159	52396	4604	8551	17102	8551
2nd	7876	68763	68763	7876	11222	22444	11222

#### Seismic force verification:

Direction	Base Seismic Forces (lbs)							Sum Wall Forces (lbs)	% Difference
	Masses			Forces		Point Seismic	Total Base Shear		
	Sum of diaphragm masses	Sum point mass	Total mass	Seismic factor	Seismic force from mass				
N-S	121159	0	121159	0.0879	10647	0	10647	10647	0.001
E-W	121159	0	121159	0.0879	10647	0	10647	10647	0.002

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## Wind Loads

Design Code: International Building Code <sup>2015</sup> 2009  
 Wind Standard: ASCE7-05 (Method 2 - All Heights)  
 Wind Data

Exposure C

Enclosure Enclosed Building

Category II

Wind Speed 85 MPH → 110 mph (0.6 ASD)

Mean Roof Height 23.77 ft

Importance Factor Iw 1

Hill Shape: No Topographic Obstructions

Velocity Coefficient  $q_z$   $0.00256 K_z K_{zt} K_d V^2 I_w$  (6-15)

Velocity Coefficient  $q_h$   $0.00256 K_h K_{zt} K_d V^2 I_w$  (6-15)

Directionality Factor  $K_d$  0.85 Table 6-4

Gust Effect Factor G 0.85 6.5.8.1

Pressures for MWFRS  $p$   $qGC_p$  (6-17)

$K_h$  0.94

North/South  $C_p$  :

Windward Wall  $C_p$  0.80

Leeward Wall  $C_p$  -0.50

(L/B) 0.41

East/West  $C_p$  :

Windward Wall  $C_p$  0.80

Leeward Wall  $C_p$  -0.28

(L/B) 2.44

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### Wind Load Distribution (North/South)

Elev. Z (ft)	K <sub>z</sub>	K <sub>zt</sub>	q <sub>z</sub> (psf)	p (Wall-Windward) (psf)
0-15	0.85	1.00	13.35	9.08
20.00	0.90	1.00	14.18	9.64
23.77	0.94	1.00	14.70	10.00

p (Wall-Leeward) (psf) -6.25

p (Roof Windward) (psf) 22.06

p (Roof Leeward) (psf) -14.70

### Wind Load Distribution (East/West)

Elev. Z (ft)	K <sub>z</sub>	K <sub>zt</sub>	q <sub>z</sub> (psf)	p (Wall-Windward) (psf)
0-15	0.85	1.00	13.35	9.08
20.00	0.90	1.00	14.18	9.64
23.77	0.94	1.00	14.70	10.00

p (Wall-Leeward) (psf) -3.48

p (Roof Windward) (psf) 22.06

p (Roof Leeward) (psf) -14.70

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### Shear line reactions and shear wall forces

Floor ID: 1st

Shear line ID	Reaction (lbs)		Shear wall ID	Shear wall forces (lbs)		R*	Wall type
	Seismic	Wind		Seismic	Wind		
1	1387	6518	1-1	561	2634	6.50	Solid wall
			1-2	827	3884	6.50	Solid wall
2	1384	6518	2-1	1384	6518	6.50	Solid wall
a	1335	2191	a-1	118	194	6.50	Solid wall
			a-2	1217	1997	6.50	Solid wall
b	1436	2191	b-1	1436	2191	6.50	Solid wall

Floor ID: 2nd

Shear line ID	Reaction (lbs)		Shear wall ID	Shear wall forces (lbs)		R*	Wall type
	Seismic	Wind		Seismic	Wind		
1	3940	6430	1-1	1259	2055	6.50	Segmented
			1-2	1422	2321	6.50	Segmented
			1-3	1259	2055	6.50	Segmented
2	3936	6430	2-1	3936	6430	6.50	Segmented
a	3933	2361	a-1	3933	2361	6.50	Segmented
b	3943	2361	b-1	1686	1010	6.50	Segmented
			b-2	2257	1351	6.50	Segmented

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**Shear Wall Schedule**

Mark	Sheathing	No. of sides	Edge Nail	Field Nail	Plate Nail	Shear Clip	Mudsill Anchors		Allowable Shear (plf)	Material	Remarks
							2X Mudsill	3X Mudsill			
1	15/32" Sheathing, plywood siding except Group 5 Species	Single	8d @ 6"	8d @ 12"	1/4"x6" SDS @ 1'-4"	A35 @ 2'-0"	5/8" x 10" @ 4'-0"	5/8" x 12" @ 4'-0"	242	SPF	1
2	15/32" Sheathing, plywood siding except Group 5 Species	Single	8d @ 4"	8d @ 12"	1/4"x6" SDS @ 1'-0"	A35 @ 1'-4"	5/8" x 10" @ 3'-0"	5/8" x 12" @ 4'-0"	350	SPF	1
3	15/32" Sheathing, plywood siding except Group 5 Species	Single	8d @ 3"	8d @ 12"	1/4"x6" SDS @ 0'-8"	A35 @ 1'-0"	5/8" x 10" @ 2'-9"	5/8" x 12" @ 3'-0"	455	SPF	1,2
5	15/32" Sheathing, plywood siding except Group 5 Species	Double	8d @ 4"	8d @ 12"	1/4"x6" SDS @ 0'-6"	A35 @ 0'-8"	5/8" x 10" @ 1'-9"	5/8" x 12" @ 2'-0"	707	SPF	1,2
7	15/32" Sheathing, plywood siding except Group 5 Species	Double	10d @ 3"	10d @ 12"	1/4"x6" SDS @ 0'-4"	A35 @ 0'-4"	5/8" x 10" @ 1'-1"	5/8" x 12" @ 1'-4"	1,116	SPF	1,2

- 1 USE PLYWOOD SHEATHING ONLY.
- 2 ALL FRAMING MEMBERS RECEIVING EDGE NAILING FROM ABUTTING PANELS SHALL NOT BE LESS THAN A SINGLE 3-INCH NOMINAL MEMBER OR TWO 2-INCH NOMINAL MEMBERS FASTENED IN ACCORDANCE WITH SECTION 2306.1 TO TRANSFER THE DESIGN SHEAR VALUE BETWEEN FRAMING MEMBERS. WOOD STRUCTURAL PANEL JOINT AND SILL PLATE NAILING SHALL BE STAGGERED IN ALL CASES.
- 3 ALL HARDWARE SHALL BE USP STRUCTURAL CONNECTORS U.O.N.

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Shear Wall Design

1st walls

Wall ID	Length (ft)	Net Height (ft)	H / W	Shear (plf)		Wall type	Allowable shear (plf)	Adjusted allowable shear (plf)		Wall Drift (in)	Hold-Down		Remarks
				Wind	Seismic			Wind	Seismic		End I	End J	
1-1	10'-8"	9'-0"											1
1-2	15'-9"	9'-0"											1
2-1	32'-0"	9'-0"											1
a-1	5'-0"	10'-0"											1
a-2	51'-6"	10'-0"											1
b-1	78'-0"	10'-0"											1

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2nd walls

Wall ID	Length (ft)	Net Height (ft)	H / W	Shear (plf)		Wall type	Allowable shear (plf)	Adjusted allowable shear (plf)		Wall Drift (in)	Hold-Down		Remarks
				Wind	Seismic			Wind	Seismic		End I	End J	
1-1	4'-6"	8'-11"	2.00	457	364	3	455	637	455	2.13	HDQ8-SDS3 4x	HDQ8-SDS3 4x	
1-2	5'-1"	8'-11"	1.77	457	364	3	455	637	455	2.03	HDQ8-SDS3 4x	HDQ8-SDS3 4x	
1-3	4'-6"	8'-11"	2.00	457	364	3	455	637	455	2.13	HDQ8-SDS3 4x	HDQ8-SDS3 4x	
2-1	14'-4"	8'-11"	0.63	447	356	3	455	637	455	1.50	HDQ8-SDS3 4x	HDQ8-SDS3 4x	
a-1	12'-0"	8'-11"	0.75	197	426	3	455	637	455	1.80	HDQ8-SDS3 4x	HDQ8-SDS3 4x	
b-1	8'-0"	8'-11"	1.12	126	274	2	350	490	350	1.56	HDQ8-SDS3 4x	HDU4-SDS2.5	
b-2	10'-8"	8'-11"	0.84	126	274	2	350	490	350	1.44	HDU4-SDS2.5	HDU4-SDS2.5	

1 Solid Wall



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# **HOLD-DOWN SCHEDULE**

Mark	Fastener	Minimum Wood Member	Anchor Bolt	Capacity (lbs)	Remarks
HDU4-SDS2.5	10-SDS 1/4" X 2.5"	(2) 2 x 4	5/8"	3285	
HDQ8-SDS3 4x	20-SDS 1/4" X 3.5"	4 x 4	7/8"	5495	

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### Uplift Calculations

**Load Cases:**

$$0.6D + W$$

$$(0.6 - 0.14S_{DS})D + 0.7pQ_E$$

**2nd Walls**

Post ID	Shear Wall	Reactions (lbs)			Wall Height (ft)	Net Uplift (lbs)	Hold Down
		DL	W	0.7E			
UP2	b-1	339	-1479	-3211	11.72	-3046	HDQ8-SDS3 4x
	1-3	202	-5351	-4262	11.72	-5229	
UP1	1-3	202	-5351	-4262	11.72	-5229	HDQ8-SDS3 4x
UP4	1-2	229	-5351	-4262	11.72	-5213	HDQ8-SDS3 4x
UP3	1-2	229	-5351	-4262	11.72	-5213	HDQ8-SDS3 4x
UP6	1-1	202	-5351	-4262	11.72	-5229	HDQ8-SDS3 4x
UP5	1-1	202	-5351	-4262	11.72	-5229	HDQ8-SDS3 4x
UP7	b-1	339	-1479	-3211	11.72	-3046	HDU4-SDS2.5
UP9	b-2	482	-1479	-3211	11.72	-2977	HDU4-SDS2.5
UP8	b-2	482	-1479	-3211	11.72	-2977	HDU4-SDS2.5
UP11	a-1	540	-2306	-4993	11.72	-4731	HDQ8-SDS3 4x
UP10	a-1	540	-2306	-4993	11.72	-4731	HDQ8-SDS3 4x
UP13	2-1	647	-5242	-4171	11.72	-4854	HDQ8-SDS3 4x
UP12	2-1	647	-5242	-4171	11.72	-4854	HDQ8-SDS3 4x

- NR indicates that no hold-down is required because there is no net uplift.
- No Selection indicates that uplift value is larger than available hold-down capacities defined in database.
- PP indicates hold-down attached to a pre-manufactured shear wall panel.

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Diaphragm Design

Floor\_ID: 1st  
 Diaphragm\_ID: D1  
 Nailing  
 Load Direction: E-W  
 Code Check  
 Diaphragm Shear: Passed

Span	Sheathing		Nailing		Min. member thickness (in)	Diaphragm type	Case ID	Effective depth (ft)		Seismic shear (plf)		Wind shear (plf)		Chord force (lbs)		Check
	Grade	Thickness (in)	Boundary	Other edges				For shear	For bending	Applied shear	Allowable shear	Applied shear	Allowable shear	Seismic	Wind	
a-b	Sheathing and Single-Floor	19/32	10d@6	10d@6	2	Unblocked	3	55.96	78.00	68	215	36	300	627	225	P

Load Direction: N-S

Span	Sheathing		Nailing		Min. member thickness (in)	Diaphragm type	Case ID	Effective depth (ft)		Seismic shear (plf)		Wind shear (plf)		Chord force (lbs)		Check
	Grade	Thickness (in)	Boundary	Other edges				For shear	For bending	Applied shear	Allowable shear	Applied shear	Allowable shear	Seismic	Wind	
1-2	Sheathing and Single-Floor	19/32	10d@6	10d@6	2	Unblocked	1	32.00	32.00	134	285	204	400	2518	3972	P

Evergreen Design Company		DESIGNED		JOB NO.	
PROJECT Ravensdale		CHECKED		SHT OF	
SUBJECT		DATE			

Floor\_ID: 2nd

Diaphragm\_ID: D1

### Nailing

Load Direction: E-W

Code Check  
Diaphragm Shear: Passed

Span	Sheathing		Nailing		Min. member thickness (in)	Diaphragm type	Case ID	Effective depth (ft)		Seismic shear (plf)		Wind shear (plf)		Chord force (lbs)		Check
	Grade	Thickness (in)	Boundary	Other edges				For shear	For bending	Applied shear	Allowable shear	Applied shear	Allowable shear	Seismic	Wind	
a-b	Sheathing and Single-Floor	19/32	10d@6	10d@6	2	Unblocked	3	77.96	77.96	71	215	30	300	562	239	P

Load Direction: N-S

Span	Sheathing		Nailing		Min. member thickness (in)	Diaphragm type	Case ID	Effective depth (ft)		Seismic shear (plf)		Wind shear (plf)		Chord force (lbs)		Check
	Grade	Thickness (in)	Boundary	Other edges				For shear	For bending	Applied shear	Allowable shear	Applied shear	Allowable shear	Seismic	Wind	
1-2	Sheathing and Single-Floor	19/32	10d@6	10d@6	2	Unblocked	1	31.96	31.96	175	285	201	400	3389	3903	P

Project: Ravensdale

Location: Roof - south header 4' - multi-span (10-21-19)

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 12.0 FT (4 + 4 + 4)

#2 - Hem-Fir - Dry Use

Section Adequate By: 35.0%

Controlling Factor: Moment

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DEFLECTIONS	Left	Center	Right
Live Load	0.02 IN L/2785	0.01 IN L/4081	0.02 IN L/2785
Dead Load	0.00 in	0.00 in	0.00 in
Total Load	0.02 IN L/2177	0.01 IN L/3960	0.02 IN L/2177
Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180			

REACTIONS	A	B	C	D
Live Load	1505 lb	4013 lb	4013 lb	1505 lb
Dead Load	540 lb	1486 lb	1486 lb	540 lb
Total Load	2045 lb	5499 lb	5499 lb	2045 lb
Bearing Length	0.92 in	2.47 in	2.47 in	0.92 in

BEAM DATA	Left	Center	Right
Span Length	4 ft	4 ft	4 ft
Unbraced Length-Top	0 ft	0 ft	0 ft
Unbraced Length-Bottom	4 ft	4 ft	4 ft
Live Load Duration Factor	1.15		
Notch Depth	0.00		

#### MATERIAL PROPERTIES

#2 - Hem-Fir

	Base Values	Adjusted
Bending Stress:	Fb = 575 psi	Fb' = 660 psi
	Cd=1.15 Cl=1.00 CF=1.00	
Shear Stress:	Fv = 140 psi	Fv' = 161 psi
	Cd=1.15	
Modulus of Elasticity:	E = 1100 ksi	E' = 1100 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ = 405 psi	Fc $\perp$ = 405 psi

Controlling Moment: -2101 ft-lb

Over right support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2, 3

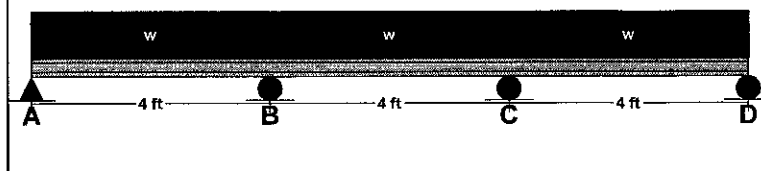
Controlling Shear: 2873 lb

At left support of span 3 (Right Span)

Created by combining all dead loads and live loads on span(s) 2, 3

Comparisons with required sections:	Req'd	Provided
Section Modulus:	38.19 in3	51.56 in3
Area (Shear):	26.76 in2	41.25 in2
Moment of Inertia (deflection):	16.66 in4	193.36 in4
Moment:	-2101 ft-lb	2836 ft-lb
Shear:	2873 lb	4428 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

	Left	Center	Right
Uniform Live Load	836 plf	836 plf	836 plf
Uniform Dead Load	330 plf	330 plf	330 plf
Beam Self Weight	8 plf	8 plf	8 plf
Total Uniform Load	1174 plf	1174 plf	1174 plf

Project: Ravensdale

Location: Roof - south header 4' - single span (10-21-19)

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 4.0 FT

#2 - Hem-Fir - Dry Use

Section Adequate By: 21.0%

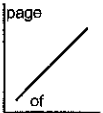
Controlling Factor: Moment

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#### DEFLECTIONS

Center

Live Load 0.02 IN L/2121

Dead Load 0.01 in

Total Load 0.03 IN L/1510

Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180

#### REACTIONS

A

B

Live Load 1672 lb 1672 lb

Dead Load 675 lb 675 lb

Total Load 2347 lb 2347 lb

Bearing Length 1.05 in 1.05 in

#### BEAM DATA

Center

Span Length 4 ft

Unbraced Length-Top 0 ft

Unbraced Length-Bottom 4 ft

Live Load Duration Factor 1.15

Notch Depth 0.00

#### MATERIAL PROPERTIES

#2 - Hem-Fir

Base Values

Adjusted

Bending Stress: Fb = 575 psi Fb' = 661 psi

Cd=1.15 CF=1.00

Shear Stress: Fv = 140 psi Fv' = 161 psi

Cd=1.15

Modulus of Elasticity: E = 1100 ksi E' = 1100 ksi

Comp.  $\perp$  to Grain: Fc  $\perp$  = 405 psi Fc  $\perp$ ' = 405 psi

Controlling Moment: 2347 ft-lb

2.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 2347 lb

At left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:

Req'd

Provided

Section Modulus: 42.6 in<sup>3</sup> 51.56 in<sup>3</sup>

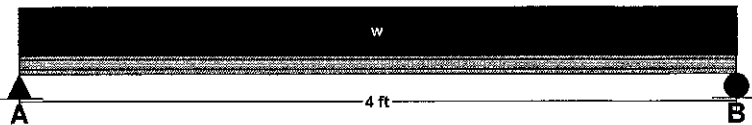
Area (Shear): 21.87 in<sup>2</sup> 41.25 in<sup>2</sup>

Moment of Inertia (deflection): 23.04 in<sup>4</sup> 193.36 in<sup>4</sup>

Moment: 2347 ft-lb 2841 ft-lb

Shear: 2347 lb 4428 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

Center

Uniform Live Load 836 plf

Uniform Dead Load 330 plf

Beam Self Weight 8 plf

Total Uniform Load 1174 plf

Project: Ravensdale  
Location: Roof - east and west headers (10-21-19)  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
( 2 ) 1.5 IN x 5.5 IN x 6.5 FT  
#2 - Hem-Fir - Dry Use  
Section Adequate By: 105.9%  
Controlling Factor: Moment

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DEFLECTIONS		Center
Live Load	0.04	IN L/1750
Dead Load	0.05	in
Total Load	0.10	IN L/820
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

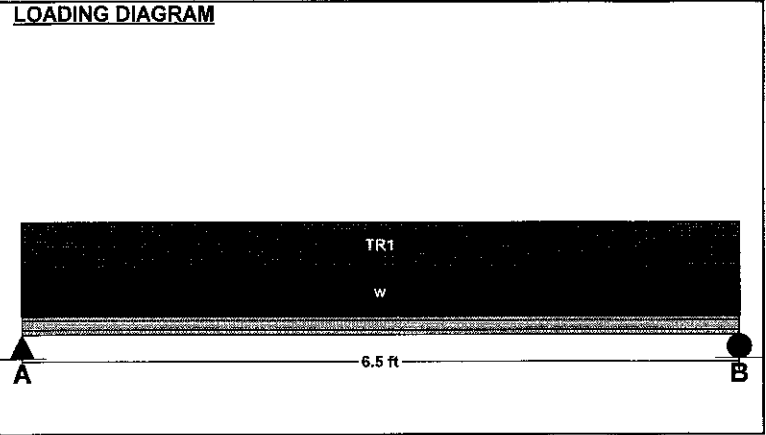
REACTIONS		A	B
Live Load	195	lb	195 lb
Dead Load	221	lb	221 lb
Total Load	416	lb	416 lb
Bearing Length	0.34	in	0.34 in

BEAM DATA		Center
Span Length	6.5	ft
Unbraced Length-Top	0	ft
Unbraced Length-Bottom	6.5	ft
Live Load Duration Factor	1.00	
Notch Depth	0.00	

MATERIAL PROPERTIES		#2 - Hem-Fir	
		Base Values	Adjusted
Bending Stress:	Fb =	850 psi	Fb' = 1105 psi
	Cd=1.00 CF=1.30		
Shear Stress:	Fv =	150 psi	Fv' = 150 psi
	Cd=1.00		
Modulus of Elasticity:	E =	1300 ksi	E' = 1300 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ =	405 psi	Fc $\perp$ ' = 405 psi

**Controlling Moment:** 676 ft-lb  
3.25 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
**Controlling Shear:** -416 lb  
6.0 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2

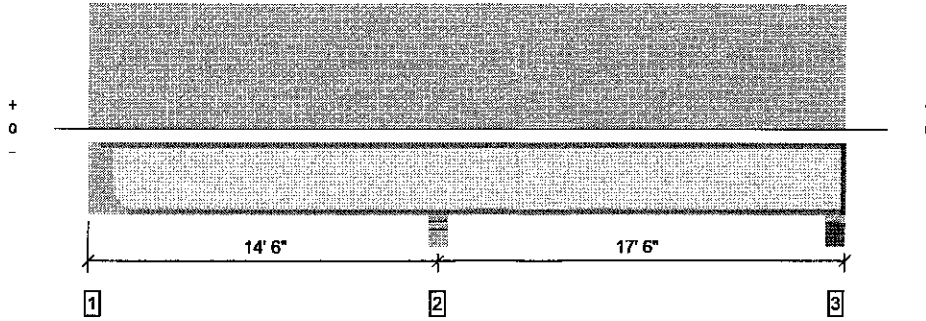
Comparisons with required sections:	Req'd	Provided
Section Modulus:	7.35 in3	15.13 in3
Area (Shear):	4.16 in2	16.5 in2
Moment of Inertia (deflection):	12.17 in4	41.59 in4
Moment:	676 ft-lb	1393 ft-lb
Shear:	-416 lb	1650 lb



UNIFORM LOADS		Center
Uniform Live Load	60	plf
Uniform Dead Load	15	plf
Beam Self Weight	3	plf
Total Uniform Load	78	plf

TRAPEZOIDAL LOADS - CENTER SPAN		One
Load Number	0	plf
Left Live Load	50	plf
Left Dead Load	0	plf
Right Live Load	50	plf
Right Dead Load	0	plf
Load Start	6.5	ft
Load End	6.5	ft
Load Length	6.5	ft

Overall Length: 32'



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal. Drawing is Conceptual

Design Results	Actual @ Location	Allowed	Result	LDF	Load Combination (Pattern)
Member Reaction (lbs)	1367 @ 14' 6"	3000 (5.25")	Passed (46%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	677 @ 14' 8 3/4"	1876	Passed (36%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	-2182 @ 14' 6"	6180	Passed (35%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.175 @ 23' 7 1/16"	0.428	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.216 @ 23' 8 1/4"	0.856	Passed (L/949)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	52	50	Passed	--	--

System : Floor  
Member Type : Joist  
Building Use : Residential  
Building Code : IBC 2015  
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at 7' 1" o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at 6' 5" o/c unless detailed otherwise.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: 1/2" Gypsum ceiling.

Supports	Bearing			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Total	
1 - Hanger on 11 7/8" SPF beam	3.50"	Hanger <sup>1</sup>	1.75" / - <sup>2</sup>	83	351/-60	434/-60	See note <sup>1</sup>
2 - Stud wall - SPF	5.50"	5.50"	3.50"	316	1052	1368	None
3 - Plate on concrete - SPF	5.50"	4.25"	1.75"	114	414/-30	528/-30	1 1/4" Rim Board

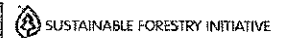
- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- <sup>1</sup> See Connector grid below for additional information and/or requirements.
- <sup>2</sup> Required Bearing Length / Required Bearing Length with Web Stiffeners

Connector: Simpson Strong-Tie Connectors							
Support	Model	Seat Length	Top Nails	Face Nails	Member Nails	Accessories	
1 - Face Mount Hanger	Connector not found	N/A	N/A	N/A	N/A		

Loads	Location (Side)	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 32'	16"	12.0	40.0	Residential - Living Areas

Member Notes
Floor: Joist

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Forte Software Operator	Job Notes
Lori Brown Evergreen Design Company pllc (360) 387-8480 loribrown@att.net	

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Forte v5.4, Design Engine: V7.1.1.3  
Ravensdale, 4te



Project: Ravensdale

Location: First - west header (10-21-19)  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
3.5 IN x 11.875 IN x 6.0 FT  
2.0E Parallam - iLevel Trus Joist  
Section Adequate By: 823.6%  
Controlling Factor: Shear

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Evergreen Design Company pllc

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#### DEFLECTIONS

##### Center

Live Load 0.00 IN L/MAX  
Dead Load 0.01 in  
Total Load 0.01 IN L/8319

Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240

#### REACTIONS

##### A

##### B

Live Load 300 lb 300 lb  
Dead Load 570 lb 570 lb  
Total Load 870 lb 870 lb  
Bearing Length 0.33 in 0.33 in

#### BEAM DATA

##### Center

Span Length 6 ft  
Unbraced Length-Top 0 ft  
Unbraced Length-Bottom 6 ft  
Live Load Duration Factor 1.00  
Notch Depth 0.00

#### MATERIAL PROPERTIES

2.0E Parallam - iLevel Trus Joist

##### Base Values

##### Adjusted

Bending Stress:  $F_b = 2900$  psi  $F_b' = 2903$  psi  
 $C_d = 1.00$   $CF = 1.00$   
Shear Stress:  $F_v = 290$  psi  $F_v' = 290$  psi  
 $C_d = 1.00$   
Modulus of Elasticity:  $E = 2000$  ksi  $E' = 2000$  ksi  
Comp.  $\perp$  to Grain:  $F_c \perp = 750$  psi  $F_c \perp' = 750$  psi

Controlling Moment: 1305 ft-lb

3.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 870 lb

At left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

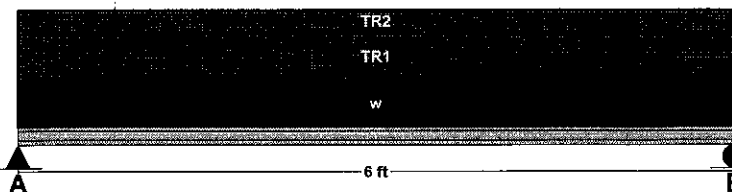
#### Comparisons with required sections:

##### Req'd

##### Provided

Section Modulus: 5.39 in<sup>3</sup> 82.26 in<sup>3</sup>  
Area (Shear): 4.5 in<sup>2</sup> 41.56 in<sup>2</sup>  
Moment of Inertia (deflection): 14.09 in<sup>4</sup> 488.41 in<sup>4</sup>  
Moment: 1305 ft-lb 19902 ft-lb  
Shear: 870 lb 8035 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

##### Center

Uniform Live Load 40 plf  
Uniform Dead Load 12 plf  
Beam Self Weight 13 plf  
Total Uniform Load 65 plf

#### TRAPEZOIDAL LOADS - CENTER SPAN

Load Number	One	Two
Left Live Load	0 plf	60 plf
Left Dead Load	150 plf	15 plf
Right Live Load	0 plf	60 plf
Right Dead Load	150 plf	15 plf
Load Start	0 ft	0 ft
Load End	6 ft	6 ft
Load Length	6 ft	6 ft

Project: Ravensdale

Location: First - north beam at garage opening in north elevation (10-21-19)  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
5.5 IN x 27.0 IN x 22.0 FT  
24F-V4 - Visually Graded Western Species - Dry Use  
Section Adequate By: 51.4%  
Controlling Factor: Moment

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#### DEFLECTIONS

##### Center

Live Load 0.28 IN L/940

Dead Load 0.15 in

Total Load 0.43 IN L/612

Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240

#### REACTIONS

##### A

##### B

Live Load 9515 lb 9515 lb

Dead Load 5117 lb 5117 lb

Total Load 14632 lb 14632 lb

Bearing Length 4.09 in 4.09 in

#### BEAM DATA

##### Center

Span Length 22 ft

Unbraced Length-Top 0 ft

Unbraced Length-Bottom 22 ft

Live Load Duration Factor 1.00

Camber Adj. Factor 1

Camber Required 0.15

Notch Depth 0.00

#### MATERIAL PROPERTIES

24F-V4 - Visually Graded Western Species

	Base Values	Adjusted
Bending Stress:	Fb = 2400 psi	Controlled by:
	Fb_cmpr = 1850 psi	Fb' = 2187 psi
	Cd=1.00 Cv=0.91	
Shear Stress:	Fv = 265 psi	Fv' = 265 psi
	Cd=1.00	
Modulus of Elasticity:	E = 1800 ksi	E' = 1800 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ = 650 psi	Fc $\perp$ = 650 psi

Controlling Moment: 80477 ft-lb

11.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 14632 lb

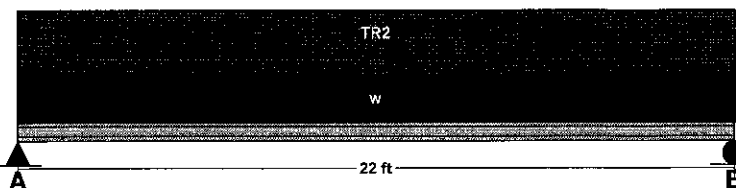
At left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

#### Comparisons with required sections:

	Req'd	Provided
Section Modulus:	441.51 in3	668.25 in3
Area (Shear):	82.82 in2	148.5 in2
Moment of Inertia (deflection):	3540.41 in4	9021.38 in4
Moment:	80477 ft-lb	121805 ft-lb
Shear:	14632 lb	26235 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

##### Center

Uniform Live Load 160 plf

Uniform Dead Load 48 plf

Beam Self Weight 32 plf

Total Uniform Load 240 plf

#### TRAPEZOIDAL LOADS - CENTER SPAN

Load Number	One	Two
Left Live Load	0 plf	705 plf
Left Dead Load	145 plf	240 plf
Right Live Load	0 plf	705 plf
Right Dead Load	145 plf	240 plf
Load Start	0 ft	0 ft
Load End	22 ft	22 ft
Load Length	22 ft	22 ft

Project: Ravensdale

Location: First - OH door header

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 15.0 IN x 18.5 FT

24F-V4 - Visually Graded Western Species - Dry Use

Section Adequate By: 91.6%

Controlling Factor: Deflection

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### DEFLECTIONS

Center

Live Load 0.32 IN L/690

Dead Load 0.11 in

Total Load 0.44 IN L/510

Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240

### REACTIONS

A

B

Live Load 3145 lb 3145 lb

Dead Load 1109 lb 1109 lb

Total Load 4254 lb 4254 lb

Bearing Length 1.19 in 1.19 in

### BEAM DATA

Center

Span Length 18.5 ft

Unbraced Length-Top 0 ft

Unbraced Length-Bottom 18.5 ft

Live Load Duration Factor 1.00

Camber Adj. Factor 1.5

Camber Required 0.17

Notch Depth 0.00

### MATERIAL PROPERTIES

24F-V4 - Visually Graded Western Species

	Base Values	Adjusted
Bending Stress:	Fb = 2400 psi	Controlled by:
	Fb_cmpr = 1850 psi	Fb' = 2360 psi
	Cd=1.00 Cv=0.98	
Shear Stress:	Fv = 265 psi	Fv' = 265 psi
	Cd=1.00	
Modulus of Elasticity:	E = 1800 ksi	E' = 1800 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ = 650 psi	Fc $\perp$ ' = 650 psi

Controlling Moment: 19674 ft-lb

9.25 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 4254 lb

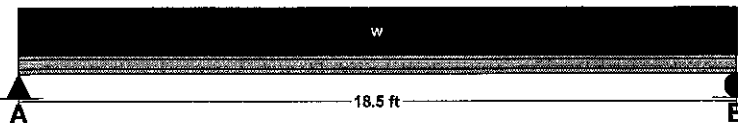
At left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

### Comparisons with required sections:

	Req'd	Provided
Section Modulus:	100.03 in3	206.25 in3
Area (Shear):	24.08 in2	82.5 in2
Moment of Inertia (deflection):	807.15 in4	1546.88 in4
Moment:	19674 ft-lb	40567 ft-lb
Shear:	4254 lb	14575 lb

### LOADING DIAGRAM



### UNIFORM LOADS

Center

Uniform Live Load	340 plf
Uniform Dead Load	102 plf
Beam Self Weight	18 plf
Total Uniform Load	460 plf

Project: Ravensdale

Location: First - interior beam over garage - steel  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(AISC 14th Ed ASD)]  
A992-50 W14x53 x 27.5 FT  
Section Adequate By: 132.9%  
Controlling Factor: Deflection

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Camano Island, WA 98282

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DEFLECTIONS	Center
Live Load	0.39 IN L/838
Dead Load	0.16 in
Total Load	0.56 IN L/594
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240	

REACTIONS	A	B
Live Load	6600 lb	6600 lb
Dead Load	2709 lb	2709 lb
Total Load	9309 lb	9309 lb
Bearing Length	1.25 in	1.25 in

BEAM DATA	Center
Span Length	27.5 ft
Unbraced Length-Top	0 ft
Unbraced Length-Bottom	27.5 ft

**STEEL PROPERTIES**

W14x53 - A992-50

**Properties:**

Yield Stress:	Fy =	50 ksi
Modulus of Elasticity:	E =	29000 ksi
Depth:	d =	13.9 in
Web Thickness:	tw =	0.37 in
Flange Width:	bf =	8.06 in
Flange Thickness:	tf =	0.66 in
Distance to Web Toe of Fillet:	k =	1.25 in
Moment of Inertia About X-X Axis:	Ix =	541 in4
Section Modulus About X-X Axis:	Sx =	77.8 in3
Plastic Section Modulus About X-X Axis:	Zx =	87.1 in3

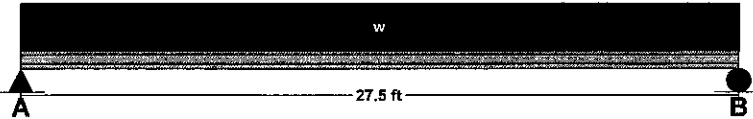
**Design Properties per AISC 14th Edition Steel Manual:**

Flange Buckling Ratio:	FBR =	6.11
Allowable Flange Buckling Ratio:	AFBR =	9.15
Web Buckling Ratio:	WBR =	30.81
Allowable Web Buckling Ratio:	AWBR =	90.55
Controlling Unbraced Length:	Lb =	0 ft
Limiting Unbraced Length - for lateral-torsional buckling:	Lp =	6.78 ft
Nominal Flexural Strength w/ safety factor:	Mn =	217315 ft-lb
Controlling Equation:	F2-1	
Web height to thickness ratio:	h/tw =	30.81
Limiting height to thickness ratio for eqn. G2-2:	h/tw-limit =	53.95
Cv Factor:	Cv =	1
Controlling Equation:	G2-2	
Nominal Shear Strength w/ safety factor:	Vn =	102860 lb

**Controlling Moment:** 63998 ft-lb  
13.75 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
**Controlling Shear:** 9309 lb  
At left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s)

Comparisons with required sections:	Req'd	Provided
Moment of Inertia (deflection):	232.31 in4	541 in4
Moment:	63998 ft-lb	217315 ft-lb
Shear:	9309 lb	102860 lb

**LOADING DIAGRAM**



**UNIFORM LOADS**

	Center
Uniform Live Load	480 plf
Uniform Dead Load	144 plf
Beam Self Weight	53 plf
Total Uniform Load	677 plf

Project: Ravensdale

Location: First - header at storage 4'  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
3.5 IN x 7.25 IN x 4.0 FT  
#2 - Hem-Fir - Dry Use  
Section Adequate By: 86.4%  
Controlling Factor: Shear

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DEFLECTIONS		Center
Live Load	0.02	IN L/2316
Dead Load	0.01	in
Total Load	0.03	IN L/1769
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

REACTIONS		A	B
Live Load	1040	lb	1040 lb
Dead Load	321	lb	321 lb
Total Load	1361	lb	1361 lb
Bearing Length	0.96	in	0.96 in

BEAM DATA		Center
Span Length	4	ft
Unbraced Length-Top	0	ft
Unbraced Length-Bottom	4	ft
Live Load Duration Factor	1.00	
Notch Depth	0.00	

#### MATERIAL PROPERTIES

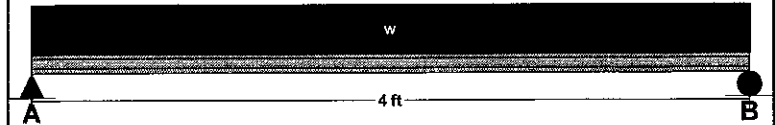
#2 - Hem-Fir

	Base Values	Adjusted
Bending Stress:	Fb = 850 psi Cd=1.00 CF=1.30	Fb' = 1105 psi
Shear Stress:	Fv = 150 psi Cd=1.00	Fv' = 150 psi
Modulus of Elasticity:	E = 1300 ksi	E' = 1300 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ = 405 psi	Fc $\perp$ ' = 405 psi

**Controlling Moment:** 1361 ft-lb  
2.0 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
**Controlling Shear:** -1361 lb  
At right support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Req'd	Provided
Section Modulus:	14.79 in3	30.66 in3
Area (Shear):	13.61 in2	25.38 in2
Moment of Inertia (deflection):	17.28 in4	111.15 in4
Moment:	1361 ft-lb	2823 ft-lb
Shear:	-1361 lb	2538 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

	Center
Uniform Live Load	520 plf
Uniform Dead Load	156 plf
Beam Self Weight	5 plf
Total Uniform Load	681 plf

Project: Ravensdale

Location: First - header at future game room 3'

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

( 2 ) 1.5 IN x 5.5 IN x 3.0 FT

#2 - Hem-Fir - Dry Use

Section Adequate By: 31.7%

Controlling Factor: Shear

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#### DEFLECTIONS

##### Center

Live Load 0.02 IN L/1669

Dead Load 0.01 in

Total Load 0.03 IN L/1279

Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240

#### REACTIONS

##### A

##### B

Live Load 960 lb 960 lb

Dead Load 293 lb 293 lb

Total Load 1253 lb 1253 lb

Bearing Length 1.03 in 1.03 in

#### BEAM DATA

##### Center

Span Length 3 ft

Unbraced Length-Top 0 ft

Unbraced Length-Bottom 3 ft

Live Load Duration Factor 1.00

Notch Depth 0.00

#### MATERIAL PROPERTIES

#2 - Hem-Fir

##### Base Values

##### Adjusted

Bending Stress:  $F_b = 850$  psi  $F_b' = 1105$  psi

$C_d = 1.00$   $CF = 1.30$

Shear Stress:  $F_v = 150$  psi  $F_v' = 150$  psi

$C_d = 1.00$

Modulus of Elasticity:  $E = 1300$  ksi  $E' = 1300$  ksi

Comp.  $\perp$  to Grain:  $F_c \perp = 405$  psi  $F_c \perp' = 405$  psi

Controlling Moment: 939 ft-lb

1.5 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -1253 lb

At right support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:

##### Req'd

##### Provided

Section Modulus: 10.2 in<sup>3</sup> 15.13 in<sup>3</sup>

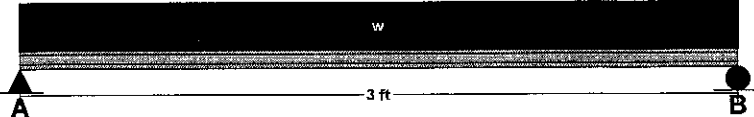
Area (Shear): 12.53 in<sup>2</sup> 16.5 in<sup>2</sup>

Moment of Inertia (deflection): 8.97 in<sup>4</sup> 41.59 in<sup>4</sup>

Moment: 939 ft-lb 1393 ft-lb

Shear: -1253 lb 1650 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

##### Center

Uniform Live Load 640 plf

Uniform Dead Load 192 plf

Beam Self Weight 3 plf

Total Uniform Load 835 plf

Project: Ravensdale

Location: First - EW beam south of stair opening

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 11.875 IN x 11.5 FT

2.0E Parallam - iLevel Trus Joist

Section Adequate By: 270.5%

Controlling Factor: Moment

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#### DEFLECTIONS

##### Center

Live Load 0.10 IN L/1428

Dead Load 0.03 in

Total Load 0.13 IN L/1054

Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240

#### REACTIONS

##### A

##### B

Live Load 1380 lb 1380 lb

Dead Load 489 lb 489 lb

Total Load 1869 lb 1869 lb

Bearing Length 0.71 in 0.71 in

#### BEAM DATA

##### Center

Span Length 11.5 ft

Unbraced Length-Top 0 ft

Unbraced Length-Bottom 11.5 ft

Live Load Duration Factor 1.00

Notch Depth 0.00

#### MATERIAL PROPERTIES

2.0E Parallam - iLevel Trus Joist

##### Base Values

##### Adjusted

Bending Stress:  $F_b = 2900$  psi  $F_b' = 2903$  psi

$C_d = 1.00$   $CF = 1.00$

Shear Stress:  $F_v = 290$  psi  $F_v' = 290$  psi

$C_d = 1.00$

Modulus of Elasticity:  $E = 2000$  ksi  $E' = 2000$  ksi

Comp.  $\perp$  to Grain:  $F_c - \perp = 750$  psi  $F_c - \perp' = 750$  psi

Controlling Moment: 5372 ft-lb

5.75 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -1869 lb

12.0 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:

##### Req'd

##### Provided

Section Modulus: 22.21 in<sup>3</sup> 82.26 in<sup>3</sup>

Area (Shear): 9.67 in<sup>2</sup> 41.56 in<sup>2</sup>

Moment of Inertia (deflection): 123.17 in<sup>4</sup> 488.41 in<sup>4</sup>

Moment: 5372 ft-lb 19902 ft-lb

Shear: -1869 lb 8035 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

##### Center

Uniform Live Load 240 plf

Uniform Dead Load 72 plf

Beam Self Weight 13 plf

Total Uniform Load 325 plf

Project: Ravensdale

Location: First - NS beam west of stair opening  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
3.5 IN x 11.875 IN x 6.5 FT  
2.0E Parallam - iLevel Trus Joist  
Section Adequate By: 443.0%  
Controlling Factor: Shear

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DEFLECTIONS		Center
Live Load	0.01	IN L/8533
Dead Load	0.00	in
Total Load	0.01	IN L/6044
Live Load Deflection Criteria: L/360    Total Load Deflection Criteria: L/240		

REACTIONS		A	B
Live Load	1062 lb	318 lb	
Dead Load	418 lb	155 lb	
Total Load	1480 lb	473 lb	
Bearing Length	0.56 in	0.18 in	

BEAM DATA		Center
Span Length	6.5	ft
Unbraced Length-Top	0	ft
Unbraced Length-Bottom	6.5	ft
Live Load Duration Factor	1.00	
Notch Depth	0.00	

#### MATERIAL PROPERTIES

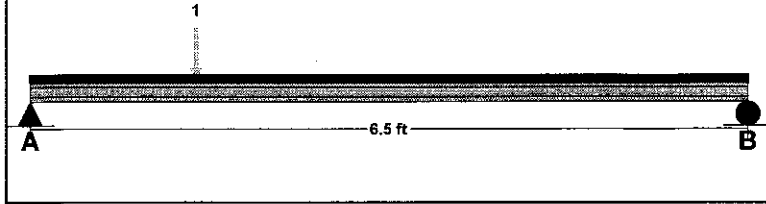
2.0E Parallam - iLevel Trus Joist

	Base Values	Adjusted
Bending Stress:	Fb = 2900 psi Cd=1.00 CF=1.00	Fb' = 2903 psi
Shear Stress:	Fv = 290 psi Cd=1.00	Fv' = 290 psi
Modulus of Elasticity:	E = 2000 ksi	E' = 2000 ksi
Comp. $\perp$ to Grain:	Fc $\perp$ = 750 psi	Fc $\perp$ ' = 750 psi

**Controlling Moment:** 2198 ft-lb  
1.49 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
**Controlling Shear:** 1480 lb  
At left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Req'd	Provided
Section Modulus:	9.08 in3	82.26 in3
Area (Shear):	7.65 in2	41.56 in2
Moment of Inertia (deflection):	20.61 in4	488.41 in4
Moment:	2198 ft-lb	19902 ft-lb
Shear:	1480 lb	8035 lb

#### LOADING DIAGRAM



#### UNIFORM LOADS

	Center
Uniform Live Load	0 plf
Uniform Dead Load	0 plf
Beam Self Weight	13 plf
Total Uniform Load	13 plf

#### POINT LOADS - CENTER SPAN

Load Number	One
Live Load	1380 lb
Dead Load	489 lb
Location	1.5 ft



Project: Ravensdale  
Location: First - EW beam south of curbless shower  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
3.5 IN x 11.875 IN x 5.5 FT  
2.0E Parallam - iLevel Trus Joist  
Section Adequate By: 542.2%  
Controlling Factor: Shear

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DEFLECTIONS		Center
Live Load	0.01	IN L/9211
Dead Load	0.00	in
Total Load	0.01	IN L/6883
Live Load Deflection Criteria: L/360    Total Load Deflection Criteria: L/240		

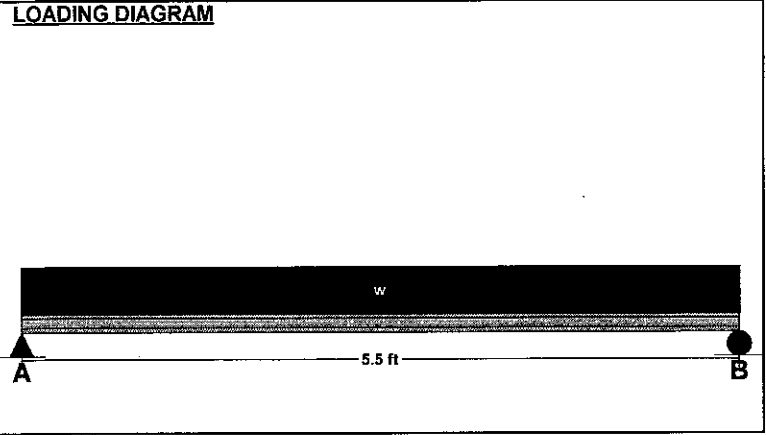
REACTIONS		A	B
Live Load	935	lb	935 lb
Dead Load	316	lb	316 lb
Total Load	1251	lb	1251 lb
Bearing Length	0.48	in	0.48 in

BEAM DATA		Center
Span Length	5.5	ft
Unbraced Length-Top	0	ft
Unbraced Length-Bottom	5.5	ft
Live Load Duration Factor	1.00	
Notch Depth	0.00	

MATERIAL PROPERTIES		Base Values	Adjusted
Bending Stress:	Fb =	2900 psi	Fb' = 2903 psi
	Cd=1.00 CF=1.00		
Shear Stress:	Fv =	290 psi	Fv' = 290 psi
	Cd=1.00		
Modulus of Elasticity:	E =	2000 ksi	E' = 2000 ksi
Comp. $\perp$ to Grain:	Fc - $\perp$ =	750 psi	Fc - $\perp$ = 750 psi

Controlling Moment: 1720 ft-lb  
2.75 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
Controlling Shear: -1251 lb  
6.0 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Req'd	Provided
Section Modulus:	7.11 in3	82.26 in3
Area (Shear):	6.47 in2	41.56 in2
Moment of Inertia (deflection):	19.09 in4	488.41 in4
Moment:	1720 ft-lb	19902 ft-lb
Shear:	-1251 lb	8035 lb



UNIFORM LOADS		Center
Uniform Live Load	340	plf
Uniform Dead Load	102	plf
Beam Self Weight	13	plf
Total Uniform Load	455	plf

Project: Ravensdale

Location: First - NS beam west of curbless shower  
Multi-Loaded Multi-Span Beam  
[2015 International Building Code(2015 NDS)]  
3.5 IN x 11.875 IN x 17.0 FT  
2.0E Parallam - iLevel Trus Joist  
Section Adequate By: 275.5%  
Controlling Factor: Deflection

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DEFLECTIONS	Center
Live Load	0.15 IN L/1354
Dead Load	0.08 in
Total Load	0.23 IN L/901
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240	

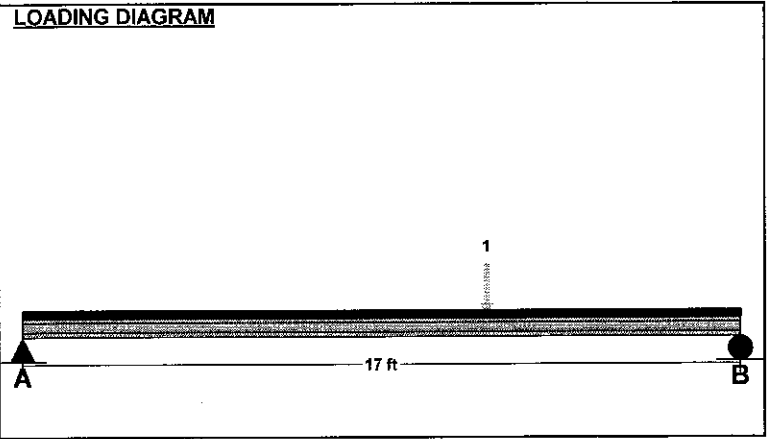
REACTIONS	A	B
Live Load	330 lb	605 lb
Dead Load	222 lb	315 lb
Total Load	552 lb	920 lb
Bearing Length	0.21 in	0.35 in

BEAM DATA	Center
Span Length	17 ft
Unbraced Length-Top	0 ft
Unbraced Length-Bottom	17 ft
Live Load Duration Factor	1.00
Notch Depth	0.00

MATERIAL PROPERTIES	Base Values	Adjusted
2.0E Parallam - iLevel Trus Joist		
Bending Stress:	Fb = 2900 psi Cd=1.00 CF=1.00	Fb' = 2903 psi
Shear Stress:	Fv = 290 psi Cd=1.00	Fv' = 290 psi
Modulus of Elasticity:	E = 2000 ksi	E' = 2000 ksi
Comp. ⊥ to Grain:	Fc ⊥ = 750 psi	Fc ⊥' = 750 psi

Controlling Moment: 5243 ft-lb  
11.05 Ft from left support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2  
Controlling Shear: -920 lb  
At right support of span 2 (Center Span)  
Created by combining all dead loads and live loads on span(s) 2

Comparisons with required sections:	Req'd	Provided
Section Modulus:	21.67 in3	82.26 in3
Area (Shear):	4.76 in2	41.56 in2
Moment of Inertia (deflection):	130.08 in4	488.41 in4
Moment:	5243 ft-lb	19902 ft-lb
Shear:	-920 lb	8035 lb



UNIFORM LOADS	Center
Uniform Live Load	0 plf
Uniform Dead Load	0 plf
Beam Self Weight	13 plf
Total Uniform Load	13 plf

<b>POINT LOADS - CENTER SPAN</b>	
Load Number	One
Live Load	935 lb
Dead Load	316 lb
Location	11 ft

**Wood Ledger**

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Description: Foundation ledger

**Code References**

Calculations per NDS 2015, IBC 2015, CBC 2016, ASCE 7-10

Load Combinations Used: ASCE 7-16

**General Information**

Ledger Width 3.50 in  
 Ledger Depth 11.250 in  
 Ledger Wood Species Hem-Fir  
 G : Specific Gravity 0.43  
 Bolt Diameter 5/8" in  
 Bolt Spacing 16.0 in  
 Cm - Wet Service Factor 1.0  
 Ct - Temperature Factor 1.0  
 Cg - Group Action Factor 1.0  
 CA - Geometry Factor 1.0

Design Method: ASD (using Service Load Combinations)

Wood Stress Grade: Hem Fir, No.2

Fb Allow 850 psi

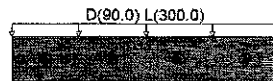
Fv Allow 150 psi

Fyb : Bolt Bending Yield 45,000 psi

Concrete as Main Supporting Member

Using 6" anchor embedment length in equations.

Using dowel bearing strength fixed at 7.5 ksi per NDS Table 11E



Analytical model actually uses 100 spans to ensure that all possible combinations of bolt location and point load location are evaluated. Final results are an envelope solution.

**Load Data**

	Dead	Roof Live	Floor Live	Snow	Wind	Seismic	Earth
Uniform Load...	90.0 plf	plf	300.0 plf	plf	plf	plf	plf
Point Load...	lbs	lbs	lbs	lbs	lbs	lbs	lbs
Spacing	in						
Offset	in						
Horizontal Shear	lbs	lbs	lbs	lbs	lbs	lbs	lbs

**Wood Ledger**

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Licensee: EVERGREEN DESIGN COMPANY

Description: Foundation ledger

**DESIGN SUMMARY****Design OK****Maximum Ledger Bending**  
Load Combination . . .

+D+L+H

Moment 57.778 ft-lb

fb : Actual Stress 9.391 psi

Fb : Allowable Stress psi

**Stress Ratio 0.01105 :1****Maximum Bolt Bearing Summary**  
Load Combination . . .

+D+L+H

Max. Vertical Load 520.0 lbs

Bolt Allow Vertical Load lbs

Max. Horizontal Load 0.0 lbs

Bolt Allow Horizontal Load 1,143.85 lbs

**Dowel Bearing Strengths**

(for specific gravity &amp; bolt diameter)

Ledger, Perp to Grain 7,500.0 ksi

Ledger, Parallel to Grain 7,500.0 ksi

Supporting Member, Perp to Grain 2,250.0 ksi

Supporting Member, Parallel to Grain 4,800.0 ksi

**Maximum Ledger Shear**

Load Combination . . .

+D+L+H

Shear 260.0 lbs

fv : Actual Stress 19.810 psi

Fv : Allowable Stress psi

**Stress Ratio 0.1321 :1**

Angle of Resultant 90.0 deg

Diagonal Component 520.0 lbs

Allow Diagonal Bolt Force 623.81 lbs

**Stress Ratio, Wood @ Bolt 0.8336 :1****Allowable Bolt Capacity**Note ! Refer to NDS Section 11.3 for Bolt Capacity calculation method.**Governing Load Combination . . +D+L+H**

Resultant Load Angle : Theta = 90.0 deg

Ktheta = 1.250 Fe theta = 623.81

**Bolt Capacity - Load Perpendicular to Grain**

Fem 7,500.0 Fes 2,250.0 Fyb 45,000.0

Re 3.333 Rt 1.714

k1 1.471 k2 2.0 k3 0.8112

Im : Eq 11.3-1 Rd = 5.0 Z = 0.0 lbs

Is : Eq 11.3-2 Rd = 5.0 Z = 984.38 lbs

Ii : Eq 11.3-3 Rd = 4.50 Z = 1,608.61 lbs

IIIm : Eq 11.3-4 Rd = 4.0 Z = 1,834.15 lbs

IIIs : Eq 11.3-5 Rd = 4.0 Z = 623.81 lbs

IV : Eq 11.3-6 Rd = 4.0 Z = 703.69 lbs

Zmin : Basic Design Value = 623.81 lbs

**Bolt Capacity - Load Parallel to Grain**

Fem 7,500.0 Fes 4,800.0 Fyb 45,000.0

Re 1.563 Rt 1.714

k1 0.8246 k2 1.303 k3 0.9325

Im : Eq 11.3-1 Rd = 4.0 Z = 0.0 lbs

Is : Eq 11.3-2 Rd = 4.0 Z = 2,625.0 lbs

Ii : Eq 11.3-3 Rd = 3.60 Z = 2,405.19 lbs

IIIm : Eq 11.3-4 Rd = 3.20 Z = 2,776.38 lbs

IIIs : Eq 11.3-5 Rd = 3.20 Z = 1,341.94 lbs

IV : Eq 11.3-6 Rd = 3.20 Z = 1,143.85 lbs

Zmin : Basic Design Value = 1,143.85 lbs

**Reference design value - Perpendicular to Grain :** $Z * CM * CD * Ct * Cg * Cdelta = 623.81 \text{ lbs}$ **Reference design value - Parallel to Grain :** $Z * CM * CD * Ct * Cg * Cdelta = 1,143.85 \text{ lbs}$

Project: Ravensdale

Location: Footing at garage beam

Footing

[2015 International Building Code(2015 NDS)]

Footing Size: 2.5 FT x 2.5 FT x 10.00 IN

Reinforcement: #4 Bars @ 7.00 IN. O.C. E/W / (4) min.

Section Footing Design Adequate

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#### FOOTING PROPERTIES

Allowable Soil Bearing Pressure:  $Q_s = 2000$  psf  
Concrete Compressive Strength:  $F'_c = 2500$  psi  
Reinforcing Steel Yield Strength:  $F_y = 40000$  psi  
Concrete Reinforcement Cover:  $c = 3$  in

#### FOOTING SIZE

Width:  $W = 2.5$  ft  
Length:  $L = 2.5$  ft  
Depth:  $\text{Depth} = 10$  in  
Effective Depth to Top Layer of Steel:  $d = 6.25$  in

#### COLUMN AND BASEPLATE SIZE

Column Type: Steel  
Column Width:  $m = 4$  in  
Column Depth:  $n = 4$  in  
Baseplate Width:  $bsw = 10$  in  
Baseplate Length:  $bsl = 10$  in

#### FOOTING CALCULATIONS

##### Bearing Calculations:

Ultimate Bearing Pressure:  $Q_u = 1504$  psf  
Effective Allowable Soil Bearing Pressure:  $Q_e = 1875$  psf  
Required Footing Area:  $A_{req} = 5.01$  sf  
Area Provided:  $A = 6.25$  sf

##### Baseplate Bearing:

Bearing Required:  $Bear = 13920$  lb  
Allowable Bearing:  $Bear-A = 276250$  lb

##### Beam Shear Calculations (One Way Shear):

Beam Shear:  $V_{u1} = 2436$  lb  
Allowable Beam Shear:  $V_{c1} = 14063$  lb

##### Punching Shear Calculations (Two Way Shear):

Critical Perimeter:  $B_o = 53$  in  
Punching Shear:  $V_{u2} = 11205$  lb  
Allowable Punching Shear (ACI 11-35):  $vc2-a = 74531$  lb  
Allowable Punching Shear (ACI 11-36):  $vc2-b = 83438$  lb  
Allowable Punching Shear (ACI 11-37):  $vc2-c = 49688$  lb  
Controlling Allowable Punching Shear:  $vc2 = 49688$  lb

##### Bending Calculations:

Factored Moment:  $M_u = 30682$  in-lb  
Nominal Moment Strength:  $M_n = 169665$  in-lb

##### Reinforcement Calculations:

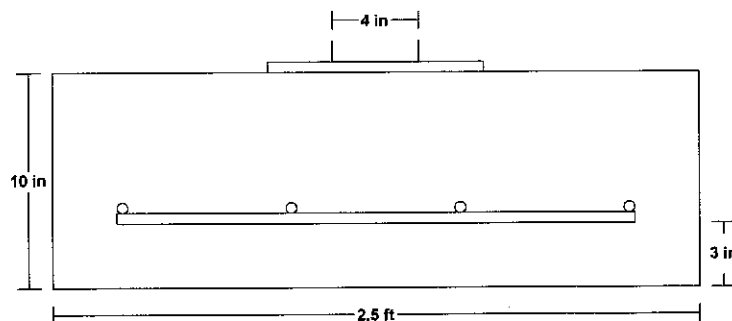
Concrete Compressive Block Depth:  $a = 0.49$  in  
Steel Required Based on Moment:  $A_s(1) = 0.14$  in<sup>2</sup>  
Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4):  $A_s(2) = 0.60$  in<sup>2</sup>  
Controlling Reinforcing Steel:  $A_{s-reqd} = 0.60$  in<sup>2</sup>  
Selected Reinforcement: #4's @ 7.0 in. o.c. e/w (4) Min.  
Reinforcement Area Provided:  $A_s = 0.79$  in<sup>2</sup>

##### Development Length Calculations:

Development Length Required:  $L_d = 15$  in  
Development Length Supplied:  $L_{d-sup} = 8.5$  in

Note: Plain concrete adequate for bending,  
therefore adequate development length not required.

#### LOADING DIAGRAM



#### FOOTING LOADING

Live Load:  $PL = 6600$  lb  
Dead Load:  $PD = 2800$  lb  
Total Load:  $PT = 9400$  lb  
Ultimate Factored Load:  $P_u = 13920$  lb  
Footing plus soil above footing weight:  $W_t = 503$  lb

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## Restrained Retaining Wall

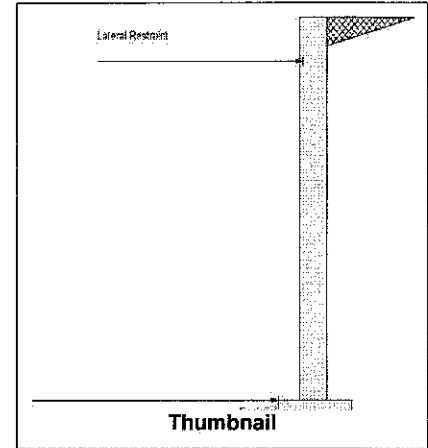
Code: IBC 2015,ACI 318-14,ACI 530-13

### Criteria

Retained Height = 9.00 ft  
Wall height above soil = 0.00 ft  
Total Wall Height = 9.00 ft  
  
Top Support Height = 8.00 ft  
  
Slope Behind Wal = 0.00  
Height of Soil over Toe = 0.00 in

### Soil Data

Allow Soil Bearing = 2,000.0 psf  
Equivalent Fluid Pressure Method  
At-rest Heel Pressure = 55.0 psf/ft  
= 200.0 psf/ft  
Passive Pressure = 110.0 pcf  
Soil Density = 0.400  
Footing||Soil Frictior = 0.400  
Soil height to ignore  
for passive pressure = 12.00 in



### Surcharge Loads

Surcharge Over Heel = 0.0 psf  
>>>Used To Resist Sliding & Overturning  
Surcharge Over Toe = 0.0 psf  
Used for Sliding & Overturning

### Axial Load Applied to Stem

Axial Dead Load = 0.0 lbs  
Axial Live Load = 0.0 lbs  
Axial Load Eccentricity = 0.0 in

### Uniform Lateral Load Applied to Stem

Lateral Load = 0.0 #/ft  
...Height to Top = 0.00 ft  
...Height to Bottom = 0.00 ft  
  
Load Type = Wind (W)  
(Strength Level)

Wind on Exposed Stem = 0.0 psf

### Adjacent Footing Load

Adjacent Footing Load = 0.0 lbs  
Footing Width = 0.00 ft  
Eccentricity = 0.00 in  
Wall to Ftg CL Dist = 0.00 ft  
Footing Type = Line Load  
Base Above/Below Soil = 0.0 ft  
at Back of Wall  
Poisson's Ratio = 0.300

### Earth Pressure Seismic Load

$K_h$  Soil Density Multiplier = 0.200 g Added seismic per unit area = 0.0 psf

### Stem Weight Seismic Load

$F_p / W_p$  Weight Multiplier = 0.000 g Added seismic per unit area = 0.0 psf

## Design Summary

Total Bearing Load = 1,807 lbs  
...resultant ecc. = 2.94 in  
  
Soil Pressure @ Toe = 241 psf OK  
Soil Pressure @ Heel = 1,566 psf OK  
Allowable = 2,000 psf  
Soil Pressure Less Than Allowable  
ACI Factored @ Toe = 289 psf  
ACI Factored @ Heel = 1,879 psf  
Footing Shear @ Toe = 0.3 psi OK  
Footing Shear @ Heel = 2.0 psi OK  
Allowable = 75.0 psi  
Reaction at Top = 832.5 lbs  
Reaction at Bottom = 1,823.8 lbs

Sliding Calcs  
Lateral Sliding Force = 1,823.8 lbs

## Concrete Stem Construction

Thickness = 8.00 in  $F_y$  = 60,000 psi  
Wall Weight = 100.0 psf  $f_c$  = 3,000 psi  
Stem is FREE to rotate at top of footing

	@ Top Support	Mmax Between Top & Base	@ Base of Wall
Design Height Above Ftg	Stem OK 8.00 ft	Stem OK 3.53 ft	Stem OK 0.00 ft
Rebar Size	# 4	# 4	# 4
Rebar Spacing	10.00 in	10.00 in	10.00 in
Rebar Placed at	Center	Center	Center
Rebar Depth 'd'	4.00 in	4.00 in	4.00 in
Design Data			
$f_b/f_b + f_a/f_a$	0.004	0.879	0.000
$\mu_{u, Actual}$	14.7 ft-#	3,574.1 ft-#	0.0 ft-#
$M_n * \phi_{i, Allowable}$	4,065.1 ft-#	4,065.1 ft-#	4,065.1 ft-#
Shear Force @ this height	1,292.5 lbs		2,227.5 lbs
Shear.....Actual	26.93 psi		46.41 psi
Shear.....Allowable	82.16 psi		82.16 psi

### Other Acceptable Sizes & Spacings:

Toe: None Spec'd -or- Not req'd:  $\mu < \phi_i * 5 * \lambda * \sqrt{f_c} * S_m$   
Heel: None Spec'd -or- Not req'd:  $\mu < \phi_i * 5 * \lambda * \sqrt{f_c} * S_m$   
Key: No key defined -or- No key defined

Vertical component of active lateral soil pressure IS  
NOT considered in the calculation of soil bearing

### Load Factors

Building Code IBC 2015,ACI  
Dead Load 1.200  
Live Load 1.600  
Earth, H 1.600  
Wind, W 1.000  
Seismic, E 1.000

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## Restrained Retaining Wall

Code: IBC 2015,ACI 318-14,ACI 530-13

### Concrete Stem Rebar Area Details

Top Support	Vertical Reinforcing	Horizontal Reinforcing
As (based on applied moment) :	0.0009 in2/ft	
(4/3) * As :	0.0012 in2/ft	Min Stem T&S Reinf Area 1.536 in2
200bd/fy : 200(12)(4)/60000 :	0.16 in2/ft	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforcing Options :
	=====	One layer of : Two layers of :
Required Area :	0.1728 in2/ft	#4@ 12.50 in #4@ 25.00 in
Provided Area :	0.24 in2/ft	#5@ 19.38 in #5@ 38.75 in
Maximum Area :	0.6503 in2/ft	#6@ 27.50 in #6@ 55.00 in

Mmax Between Ends	Vertical Reinforcing	Horizontal Reinforcing
As (based on applied moment) :	0.2158 in2/ft	
(4/3) * As :	0.2877 in2/ft	Min Stem T&S Reinf Area 0.857 in2
200bd/fy : 200(12)(4)/60000 :	0.16 in2/ft	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforcing Options :
	=====	One layer of : Two layers of :
Required Area :	0.2158 in2/ft	#4@ 12.50 in #4@ 25.00 in
Provided Area :	0.24 in2/ft	#5@ 19.38 in #5@ 38.75 in
Maximum Area :	0.6503 in2/ft	#6@ 27.50 in #6@ 55.00 in

Base Support	Vertical Reinforcing	Horizontal Reinforcing
As (based on applied moment) :	0 in2/ft	
(4/3) * As :	0 in2/ft	Min Stem T&S Reinf Area 0.679 in2
200bd/fy : 200(12)(4)/60000 :	0.16 in2/ft	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforcing Options :
	=====	One layer of : Two layers of :
Required Area :	0.1728 in2/ft	#4@ 12.50 in #4@ 25.00 in
Provided Area :	0.24 in2/ft	#5@ 19.38 in #5@ 38.75 in
Maximum Area :	0.6503 in2/ft	#6@ 27.50 in #6@ 55.00 in

### Footing Strengths & Dimensions

Toe Width	=	0.67 ft
Heel Width	=	1.33
Total Footing Width	=	2.00
Footing Thickness	=	10.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f <sub>c</sub> =	2,500 psi	F <sub>y</sub> = 60,000 psi
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	=	2.00 in @ Btm. = 3.00 in

### Footing Design Results

	Toe	Heel
Factored Pressure	= 289	1,879 psf
Mu' : Upward	= 105	376 ft-#
Mu' : Downward	= 34	294 ft-#
Mu : Design	= 71	-81 ft-#
Actual 1-Way Shear	= 0.31	2.05 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Min footing T&S reinf Area	0.43	in2
Min footing T&S reinf Area per foot	0.22	in2 /ft
If one layer of horizontal bars:	If two layers of horizontal bars:	
#4@ 11.11 in	#4@ 22.22 in	
#5@ 17.22 in	#5@ 34.44 in	
#6@ 24.44 in	#6@ 48.89 in	

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## Restrained Retaining Wall

Code: IBC 2015,ACI 318-14,ACI 530-13

### Summary of Forces on Footing : Slab RESISTS sliding, stem is PINNED at footing

#### Forces acting on footing soil pressure

(taking moments about front of footing to find eccentricity)

Surcharge Over Heel	=	lbs	ft	ft-#
Axial Dead Load on Stem	=	lbs	ft	ft-#
Soil Over Toe	=	lbs	ft	ft-#
Adjacent Footing Load	=	lbs	ft	ft-#
Surcharge Over Toe	=	lbs	ft	ft-#
Stem Weight	=	900.0 lbs	1.00 ft	903.0 ft-#
Soil Over Heel	=	656.7 lbs	1.67 ft	1,095.6 ft-#
Footing Weight	=	250.0 lbs	1.00 ft	250.0 ft-#
<b>Total Vertical Force</b>	=	<b>1,806.7 lbs</b>	<b>Moment =</b>	<b>2,248.6 ft-#</b>
<b>Net Mom. at Stem/Ftg Interface</b>	=			<b>-441.9 ft-#</b>
<b>Allow. Mom. @ Stem/Ftg Interface</b>	=			<b>2,540.7 ft-#</b>
<b>Allow. Mom. Exceeds Applied Mom.?</b>				<b>Yes</b>
<b>Therefore Uniform Soil Pressure</b>	=			<b>903.4 psf</b>

Vertical component of active lateral soil pressure IS NOT considered in  
the calculation of Sliding Resistance.